

ROBOT TCP POSITIONING WITH VISION

Accuracy Estimation of a Robot Visual Control System

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Abstract: Calibrated 3D visual servoing has not fully matured as a industrial technology yet, and in order to widen its use in industrial applications its technological capability must be precisely known. Accuracy and repeatability are two of the crucial parameters in planning of any robotic task. In this paper we describe a procedure to evaluate the 2D and 3D accuracy of a robot stereo vision system consisting of two identical 1 Megapixel cameras, and present the results of the evaluation.

1 INTRODUCTION

In the last decades, more and more robots applications were used in industrial manufacturing which was accompanied by an increased demand for versatility, robustness and precision. The demand was mostly satisfied by increasing the mechanical capabilities of robot parts. For instance, to meet the micrometric positioning requirements, stiffness of the robot's arms was increased, high precision gears and low backlash joints introduced, which often led to difficult design compromises such as the request to reduce inertia and increase stiffness. This results in approaching the mechanical limits and increased cost of robots decreasing the competitiveness of the robot systems on the market (Arflex, 2005).

Lately, the robot producers have put much effort into incorporating visual and other sensors to the actual industrial robots thus providing a significant improvement in accuracy, flexibility and adaptability. Vision is still one of the most promising sensors (Ruf and Horaud, 1999) in real robotic 3D servoing issues (Hutchinson et al., 1995). It has been vastly investigated for the last two decades in laboratories but it's only now that it finds its way to industrial implementation (Robson, 2006) in contrast to machine vision which became a well established industry in the last years (Zuech, 2000). There are many reasons for this. The vision systems used with the robots must satisfy a few constraints that differ them from a machine vision measuring systems. First of all, the camera working distances

are much larger, especially with larger robots that can reach several meters. Measuring at such distances with high precision requires much higher resolution which very soon reaches its technological and price limits. For example, nowadays 4 Megapixel cameras are the state of the art in vision technology but are not affordable in many robotic applications since their price almost reaches the robot price. The dynamics of the industrial processes requires high frame rates which in connection with real time processing puts another difficult constraint on system integrators. The unstructured industrial environment with changing environmental lighting is another challenge for the robot vision specialists.

When designing the vision system within robot applications it is very important to choose the optimal equipment for the task and to get maximal performance out of each component. In the paper we represent a procedure for the precision estimation of a calibrated robot stereo vision system in 2D and 3D environment. Such a system can be used in visual servoing applications for precise tool center point (TCP) positioning.

2 METHODOLOGY

Four types of accuracy tests were performed: a static 2D test, a dynamic 2D test, a static 3D test, and a dynamic 3D test. Throughout all the tests, an array of 10 infrared light emitting diodes (IR-LED) was used to establish its suitability for being used as a

marker and a calibration pattern in the robot visual servoing applications.

Within the static 2D test, we were moving the IR-LED array with the linear drive perpendicular to the camera optical axes and measured the increments in the image. The purpose was to detect the smallest linear response in the image. The IR-LED centroids were determined in two ways: on binary images and on grey-level images as centers of mass. During image grabbing the array did not move thus eliminating any dynamic effects. We averaged the movement of centroids of 10 IR-LEDs in a sequence of 16 images and calculated the standard deviation to obtain accuracy confidence intervals. With the dynamic 2D test shape distortions in the images due to fast 2D movements of linear drive were investigated. We compared a few images of IR-LED array taken during movement to statically obtained ones which provided information of photocenter displacements and an estimation of dynamic error.

We performed the 3D accuracy evaluation with 2 fully calibrated cameras in a stereo setup. Using again the linear drive, the array of IR-LEDs was moved along the line in 3D space with different increments and the smallest movement producing a linear response in reconstructed 3D space was sought. In the 3D dynamic test, we attached the IR-LED array to the wrist of an industrial robot, and dynamically guided it through some predefined points in space and simultaneously recorded the trajectory with fully calibrated stereo cameras. We compared the reconstructed 3D points from images to the predefined points fed to robot controller.

3 TESTING SETUP

The test environment consisted of:

- PhotonFocus MV-D1024-80-CL-8 camera with CMOS sensor and framerate of 75 fps at full resolution (1024x1024 pixels),
- Active Silicon Phoenix-DIG48 PCI frame grabber,
- Moving object (IR-LED array) at approximate distance of 2m. The IR-LED array (standard deviation of IR-LED accuracy is below 0.007 pixel, as stated in (Papa and Torkar, 2006)) fixed to Festo linear guide (DGE-25-550-SP) with repetition accuracy of +/-0.02mm.

For then static 2D test the distance from camera to a moving object (in the middle position) that moves perpendicularly to optical axis was 195cm; camera field-of-view was 220cm, which gives pixel size of 2.148mm; Schneider-Kreuznach lens

CINEGON 10mm/1,9F with IR filter; exposure time was 10.73ms, while frame time was 24.04ms, both obtained experimentally.

For the dynamic 2D test conditions were the same as in static test, except the linear guide was moving the IR-LED array with a speed of 460mm/s and the exposure time was 1ms.

In the 3D reconstruction test the left camera distance to IR-LED array and right camera distance to IR-LED array were about 205cm; baseline distance was 123cm; Schneider-Kreuznach lens CINEGON 10mm/1,9F with IR filter; Calibration region-of-interest (ROI): 342 x 333 pixels; Calibration pattern: 6 x 8 black/white squares; Calibration method (Zhang, 1998); Reconstruction method (Faugeras, 1992). The reconstruction was done off-line and the stereo correspondence problem was considered solved due to a simple geometry of the IR-LED array and is thus not addressed here.

For the 3D dynamic test, an ABB industrial robot IRB 140 was used with the standalone fully calibrated stereo vision setup placed about 2m away from its base and calibrated the same way as before. The robot wrist was moving through the corners of an imaginary triangle with side length of approximately 12cm. The images were taken dynamically when the TCP was passing the corner points and reconstructed in 3D with an approximate speed of 500mm/s. The relative length of such triangle sides were compared to the sides of a statically-obtained and reconstructed triangle. The robot native repeatability is 0.02 mm and its accuracy is 0.01mm.

4 RESULTS

4.1 2D Accuracy Tests

The results of the evaluation tests are given below. Tests include the binary and grey-level centroids. For each movement increment the two figures are presented, as described below.

Pixel difference between the starting image and the consecutive images (at consecutive positions) – for each position the value is calculated as the average displacement of all 10 markers, while their position is calculated as the average position in the sequence of the 16 images grabbed at each position in static conditions. The lines in these figures should be as straight as possible.

The 0.01mm, 0.1mm, and 1mm increments for 2D tests are presented in Figure 1.

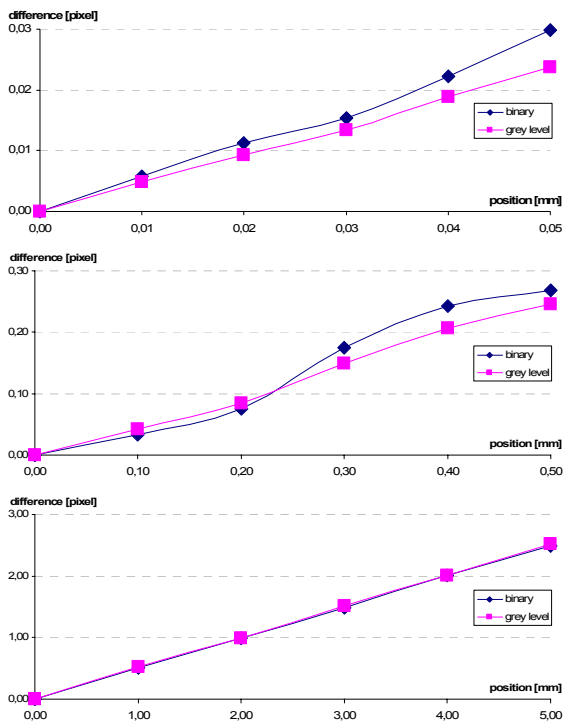


Figure 1: Pixel difference for 0.01mm (top), 0.1mm (middle), and 1mm (bottom) increments.

Figure 2 compares normalized pixel differences in grey-level images of a single marker.

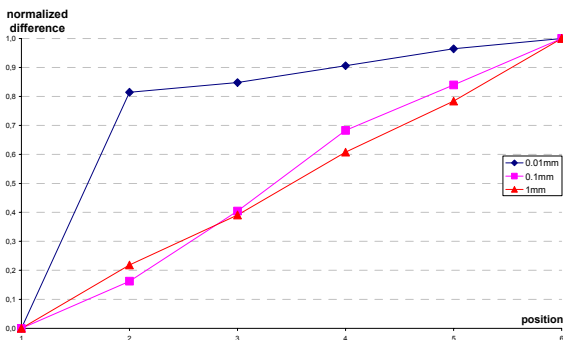


Figure 2: Normalized differences of grey-level images for each position comparing different increments.

A linear regression model was applied to measured data, and the R^2 values calculated to assess the quality of fit. The results are presented in Table 1 for 2D tests and in Table 2 for 3D tests. The R^2 value can be interpreted as the proportion of the variance in y attributable to the variance in x (see Eqn. 1), where 1 stands for perfect matching (fit) and a lower value denotes some deviations.

$$R^2 = \left(\frac{\sum (x - \bar{x})(y - \bar{y})}{\sqrt{\sum (x - \bar{x})^2 \sum (y - \bar{y})^2}} \right)^2 \quad (1)$$

Considering the R^2 threshold of 0.994 we were able to detect increments of the moving object in the range of 1/5 of a pixel. The value of the threshold is set to the value that gives a good enough approximation of the linear regression model, to ensure the applicable results of the measurements.

Table 1: Comparison of standard deviations and R^2 values for different moving increments in 2D.

increments [mm]	standard deviation [mm]		R^2	
	binary	grey-level	binary	grey-level
0.01	0.045	0.027	0.4286	0.6114
0.1	0.090	0.042	0.8727	0.9907
1	0.152	0.069	0.9971	0.9991

The dynamic 2D test showed that when comparing the centers of the markers of the IR-LED array and the pixel areas of each marker in statically and dynamically (linear guide moving at full speed) grabbed images there is a difference in center positions and also the areas of markers in dynamically grabbed images are slightly larger than those of statically grabbed images.

Table 2 presents the differences of the centers of the markers, and difference in sizes of the markers of the statically and dynamically grabbed images.

Table 2: Comparison of the images grabbed in static and dynamic mode.

	X	Y	width	height	area
static	484.445	437.992	6	6	27
dynamic	484.724	437.640	7	6	32

Regarding the results presented in Table 2, the accuracy of the position in direction x of dynamically grabbed images comparing to statically grabbed is in the range of 1/3 of a pixel, due to the gravity centre shift of pixel area of marker during the movement of the linear guide.

4.2 3D Reconstruction Tests

We tested the static relative accuracy of the 3D reconstruction of the IR-LED array movements by linear drive. The test setup consisted of the two calibrated Photonfocus cameras focused on the IR-

LED array attached to the linear drive which exhibited precise movements of 0.01mm, 0.1mm and 1mm. The mass centre points of 10 LEDs were extracted in 3D after each movement and relative 3D paths were calculated and compared to the linear drive paths. Only grey-level images were considered, due to the better results obtained in 2D tests, as stated in Figure 2 and in Table 1. The 0.01mm, 0.1mm, and 1mm increments for the 3D tests are presented in Figure 3.

The accuracy in 3D is lower than in the 2D case, due to calibration and reconstruction errors, and according to the tests performed it is approximately 1/2 of a pixel.

Table 4 presents the results of the 3D dynamic tests where the triangle area and side lengths a , b and c , reconstructed from dynamically-obtained images were compared to static reconstruction of the same triangles. 10 triangles were compared, each formed by a diode in IR-LED array. The average lengths and the standard deviations are presented.

Table 3: Comparison of standard deviations and R^2 values for different moving increments in 3D.

increments [mm]	standard deviation [mm]	R^2
0.01	0.058	0.7806
0.1	0.111	0.9315
1	0.140	0.9974

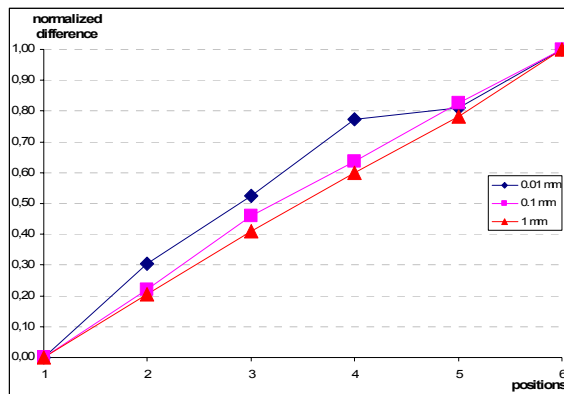


Figure 3: Pixel difference in the 3D reconstruction.

Table 4: comparison of static and dynamic triangles. All measurements are in mm.

	\bar{a}	σ	\bar{b}	σ	\bar{c}	σ
static	193.04	12.46	89.23	2.77	167.84	12.18
dynamic	193.51	12.43	89.03	2.77	167.52	12.03

We observe a significant standard deviation (up to 7%) of triangle side lengths which we ascribe to

lens distortions since it is almost the same in the dynamic and in the static case. The images and the reconstruction in dynamic conditions vary only a little in comparison to static ones.

5 CONCLUSIONS

We performed the 2D and 3D accuracy evaluation of the 3D robot vision system consisting of 2 identical 1 Megapixel cameras. The measurements showed that the raw static 2D accuracy (without any subpixel processing approaches and lens distortion compensation) is confidently as good as 1/5 of a pixel. However, this is reduced to 1/2 of a pixel when image positions are reconstructed in 3D due to reconstruction errors.

In the dynamic case, the comparison to static conditions showed that no significant error is introduced with moving markers in both, 2D and 3D environment. For the speed level of an industrial robot the accuracy is though not reduced significantly.

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REFERENCES

- Arflex European FP6 project official home page: <http://www.arflexproject.eu>
- Faugeras, O., 1992. *Three-Dimensional Computer Vision: A geometric Viewpoint*, The MIT Press.
- Hutchinson, S., Hager, G., Corke, P.I., 1995. A tutorial on visual servo control, *Yale University Technical Report*, RR-1068.
- Papa, G., Torkar, D., 2006. Investigation of LEDs with good repeatability for robotic active marker systems, *Jožef Stefan Institute technical report*, No. 9368.
- Robson, D., 2006. Robots with eyes, *Imaging and machine vision-Europe*, Vol. 17, pp. 30-31.
- Ruf, A., Horaud, R., 1999. Visual servoing of robot manipulators, Part I: Projective kinematics, *INRIA technical report*, No. 3670.
- Zhang, Z., 1998. A flexible new Technique for Camera Calibration, *Technical report*, MSRTR-98-71.
- Zuech, N., 2000. *Understanding and applying machine vision*, Marcel Dekker Inc.