# PRACTICAL ILLUMINATION CORRECTION OF SATELLITE IMAGERY IN CONSIDERATION OF ANISOTROPIC SKYLIGHT COMPONENT 

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## 1. INTRODUCTION

In satellite images over rugged terrain, we can find some topographic effect entangled with atmospheric effects [1]. Without correcting these effects, it is difficult to evaluate the satellite images for land cover classification or multi-temporal monitoring of natural environment.

Iikura[2] derived a unified simple correction formula $(D N-B) /(\cos \beta+C)$ from a physical model of signal detected by sensor on board. Although either of the parameters $B$ or $C$ is ignored in the practical illumnation correction such as C correction method [3], and modified cosine method [4], both methods seem to work well for satellite images with high sun elevation by estimating one of these parameters from regression of digital nunbers ( $D N s$ ) to cosine of solar incident angle ( $\beta$ ).

In this paper, we will estimate these parameters based on the radiative transfer equation (6s) [5] and exact calculation of topographical parameters such as sky view factor. It will be shown that the parameter $C$ becomes smaller than we expected when we take account of an anisotropic skylight component which is propotional to $\cos \beta$.

## 2. PHYSICAL BACKGROUND

For estimating surface reflectance of a target point from a satellite image, we have to evaluate various possible radiation and irradiation sources. At-sensor radiation $\left(L_{s}\right)$ of the target pixel consists of the reflected irradiation $\left(I_{o}\right)$, the path-radiance $\left(L_{p}\right)$ and background radiation $\left(L_{b}\right)$ as $L_{s}=T_{s} \cdot \rho \cdot I_{o}+L p+L_{b}$ where $\rho$ is the target reflectance, $s$ is the sensor scan angle, and $T_{s}$ is the transmittance from target to satellite. The target irradiation $\left(I_{o}\right)$ is also broken down into the direct solar beam, the diffuse sky irradiation $E_{d}$ and the reflected irradiation from adjacent slope $E_{t}$ as $I_{o}=E_{o} T_{\theta} \cos \beta+E_{d}+E_{t}$ where $T_{\theta}$ is the transmittance from the sun to the target, $\theta$ is the solar zenith angle.

From these relations, we have the reflectance as follows

$$
\rho=\frac{L_{s}-L p-L_{b}}{T_{s}\left(E_{o} T_{\theta} \cos \beta+E_{d}+E_{t}\right)}
$$

For practical corection scheme, let us use the digital number instead of the reflectance and radiation. Then we have $D N^{\prime}=$ $(D N-B) /(\cos \beta+C)$ where $D N$ is an original digital number and $D N^{\prime}$ is a corected digital number, which could be regarded as the conventional $C$ correction method. It should be also noted that the diffuse sky component $E_{d}$ is not isotropic. Hays [6] proposed to use the following expression,

$$
E_{d}=E_{d}^{h}\left\{T_{\theta}^{\prime} \cos \beta+\left(1-T_{\theta}^{\prime} \cos \theta\right) V_{d}\right\}
$$

where $E_{d}^{h}$ is the diffuse sky component for flat surface, $V_{d}$ is the terrain configuration factor, and $T_{\theta}^{\prime}$ is the transmittance by scattering (no absorption).

Then, the correction parameters $B$ and $C$ are related to the physical quantities as follows,

$$
\begin{gathered}
B=a+b \times\left(L_{p}+L_{b}\right) \\
C=\frac{E_{d}^{h}\left(1-T_{\theta}^{\prime} \cos \theta\right) V_{d}+E_{t}}{E_{o} T_{\theta}+E_{d}^{h} T_{\theta}^{\prime}}
\end{gathered}
$$

In the case of isotropic sky component, the parameter C becomes $C=\left(E_{d}+E_{t}\right) / E_{o} T_{\theta}$ as shown by Iikura[2].

## 3. PARAMETER ESTIMATION W ITH ANISOTROPIC SKYLIGHT COMPONENT

A radiative transfer code (6S) for flat terrain is used for Landsat TM image (June $16,1985, \mathrm{p} 107 \mathrm{r} 32$ ) under the following conditions: mid latitude summer atmosphere with marine type aerosol of 30 km horizontal visibility, sun elevation angle of $62.7^{\circ}$, and a normal vegetation for ground surface.

### 3.1 Sky view factor $V_{d}$

We calculate angles $H_{\phi}$ from zenith to horizon for 64 azimuth directions $\phi$, and sum sky lights from these directions to obtain $V_{d}$. As this operation is performed to every pixels in the image, we need an efficient algorithm [2].The result would be compared to that of the conventional approximation $V_{d}=(1+\cos S) / 2$ where $S$ is the slope.

### 3.2 Reflected irradiation

Radiation from a pixel $P$ contributes to irradiation at the target pixel $M$ as

$$
L_{P M}=\left(L_{p} d S_{M} \cos T_{M} d S_{P} \cos T_{P}\right) / r_{M P}^{2}
$$

where $d S_{M} d S_{P}$ denote the areas of pixel $P, T_{M}$ and $T_{P}$ are angles between surface normal and line $M P$, and $r_{M P}$ is a distance between pixel M and pixel $P$. If we assume lambertian surface, $L_{P}$ can be obtained by calibrating a digital number of pixel $P$ into radiation. Reflected radiance at pixel $M$ is a sum of the $L_{P M}$ for pixels which is visible from $M$, that is, viewshed of $M$. Therefore, we have to obtain the viewshed for this calculation [2].

## 4. CONCLUSION

Table 1 shows that the correction parameter C for anisotropic sky light component is small for every bands, and seems negligible in the case of summer data with high sun elevation. In infrared bands, however, it is noted the deviation due to $E_{d}$ is large as shown in Fig.1. For the image with low sun elevation, exact treatment like this might be required.

Table 1. Correction parameters calculated based on physical model

| Band | 1 | 2 | 3 | 4 | 5 | 7 |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| B | 71.54 | 23.38 | 18.84 | 28.73 | 20.20 | 7.83 |
| C (anisotropic) | 0.04591 | 0.03433 | 0.02639 | 0.06460 | 0.03611 | 0.02145 |
| C (isotropic) | 0.26973 | 0.21933 | 0.19035 | 0.21717 | 0.15682 | 0.12665 |

## 5. REFERENCES

[1] D. Tanre C. Proy and P.Y. Deshamps, "Evaluation of topographic effects in remotely sensed data," Remote Sensing of Environment, vol. 30, pp. 21-32, 1989.
[2] Y. Iikura, "Precise evaluation of topographic effects in satellite imagery for illumination correction," in Proceedings of IGARSS 2008 (CD-ROM). IEEE, 2008, Boston, U.S.A.
[3] P.M. Teillet et al., "On the slope-aspect correction of multispectral scanner data," Canadian J. Remote Sensing, vol. 8, pp. 84-106, Feburuary 1982.
[4] Y. Iikura, "Optimization of geometric correction of landsat tm images using digital elevation model," J. Remote Sensing Society of Japan, vol. 22, pp. 189-195, May 2002, in Japanese with English ABSTRACT.
[5] E.F. Vermote et al., "Second simulation of the satellite signal in the solar spectrum, 6s: an overview," IEEE TGRS, vol. 35, pp. 675-686, March 1997.
[6] J.E. Hay and D.C. Mackay, "Estimating solar irradiance on inclined surfaces: a review and assessment of methodologies," Int. J. Solar Energy, vol. 3, pp. 203-240, March 1985.

